



# ONE STEP KINETIC MODEL OF COAL PYROLYSIS FOR CFD APPLICATIONS

Tiziano Maffei, Eliseo Ranzi, Alessio Frassoldati and Tiziano Faravelli

Department of Chemistry, Materials, and Chemical Engineering, Politecnico di Milano, P.zza Leonardo da Vinci 32, 20133 Milano, Italy

## OBJECTIVE

Aim of this work is the development of a simplified kinetic model for coal devolatilization, suitable for CFD applications, able not only to describe the conversion of coal but also the relative yields of solid, tar and gaseous species, in term of hydrocarbon, sulphur and nitrogen compounds.

## DETAILED MODEL OF COAL PYROLYSIS

Three different detailed kinetic models have been considered:

1. Kinetic model for the release of Hydrocarbon species [1].
2. Kinetic model for the release of Sulfur compounds [2].
3. Kinetic model for the release of Nitrogen compound.

### Nitrogen Kinetic Model

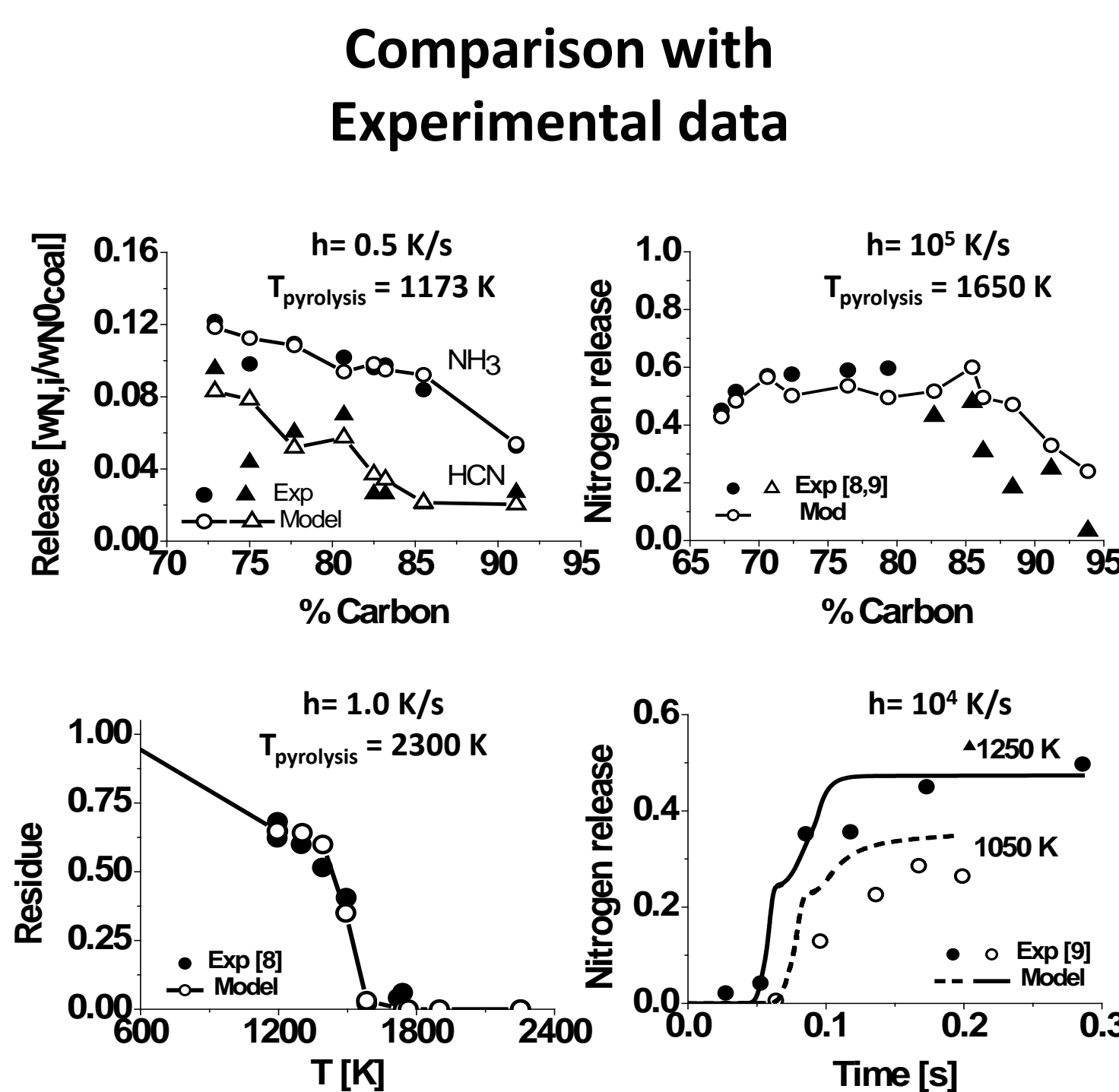
#### Nitrogen Matrix Characterization:

Has been applied the same criterion used to characterize the effect solid phase composition on the release of hydrocarbon species [3,4].

#### Kinetic Mechanism

		A (*)	E <sub>ATT</sub> (**)
1	COAL-N <sub>1</sub> → 0.1 NH <sub>3</sub> * + 0.05 HCN* + 0.85 N <sub>CHAR</sub>	9.0×10 <sup>7</sup>	40000
2	COAL-N <sub>1</sub> → N <sub>TAR</sub> *	1.0×10 <sup>8</sup>	40000
3	COAL-N <sub>1</sub> → 0.05 NH <sub>3</sub> * + 0.3 HCN* + 0.65 N <sub>CHAR</sub>	1.6×10 <sup>15</sup>	75000
4	COAL-N <sub>1</sub> → N <sub>TAR</sub> *	1.0×10 <sup>14</sup>	75000
5	COAL-N <sub>2</sub> → 0.15 NH <sub>3</sub> * + 0.03 HCN* + 0.82 N <sub>CHAR</sub>	7.6×10 <sup>10</sup>	36000
6	COAL-N <sub>2</sub> → N <sub>TAR</sub> *	5.0×10 <sup>10</sup>	36000
7	COAL-N <sub>2</sub> → 0.15 NH <sub>3</sub> * + 0.3 HCN* + 0.55 N <sub>CHAR</sub>	3.0×10 <sup>17</sup>	63000
8	COAL-N <sub>2</sub> → N <sub>TAR</sub> *	4.0×10 <sup>17</sup>	63000
9	COAL-N <sub>3</sub> → 0.15 NH <sub>3</sub> * + 0.1 HCN* + 0.75 N <sub>CHAR</sub>	5.0×10 <sup>18</sup>	61000
10	COAL-N <sub>3</sub> → N <sub>TAR</sub> *	1.6×10 <sup>19</sup>	33000
11	COAL-N <sub>3</sub> → 0.15 NH <sub>3</sub> * + 0.1 HCN* + 0.75 N <sub>CHAR</sub>	5.0×10 <sup>18</sup>	61000
12	COAL-N <sub>3</sub> → N <sub>TAR</sub> *	2.0×10 <sup>18</sup>	61000
13	N <sub>CHAR</sub> * + N <sub>TAR</sub> * → 0.05 NH <sub>3</sub> * + 0.1 HCN* + 1.85 N <sub>CHAR</sub>	2.1×10 <sup>6</sup>	32500
14	N <sub>TAR</sub> * → N <sub>TAR</sub> *	3.0×10 <sup>8</sup>	32500
15	NH <sub>3</sub> * → NH <sub>3</sub>	1.0×10 <sup>3</sup>	23000
16	HCN* → HCN	4.0×10 <sup>2</sup>	23000
17	N <sub>CHAR</sub> * → CHAR <sub>C</sub> +HCN	2.0×10 <sup>9</sup>	80000

\*Units: cal, mol, K, s, m



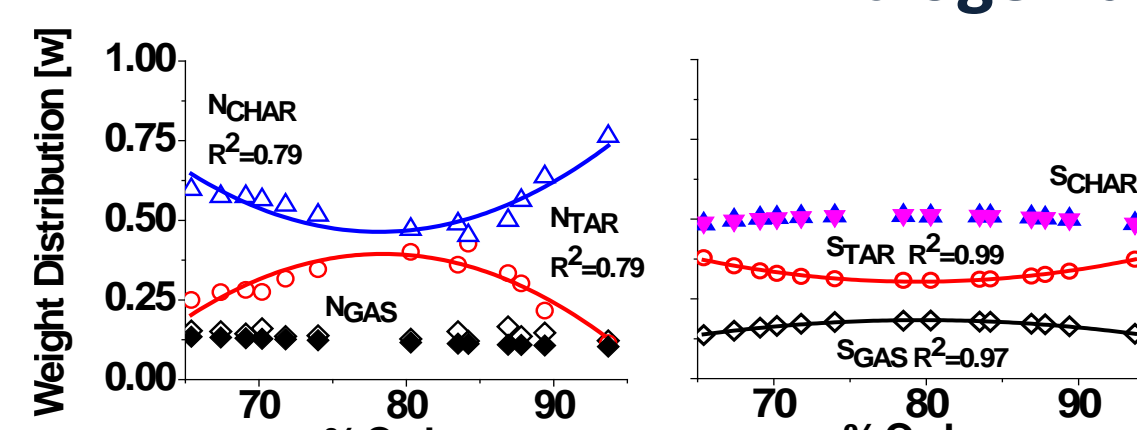
## STOICHIOMETRIC COEFFICIENTS

### Hydrocarbon release mechanism (high temperature)

	CHAR <sub>C</sub>	H <sub>2</sub>	CH <sub>4</sub>	C <sub>2-5</sub>	BTX	CO	H <sub>2</sub> O	CO <sub>2</sub>	TAR <sub>1</sub>	TAR <sub>2</sub>	TAR <sub>3</sub>
COAL <sub>1</sub>	5.13	1.50	0.38	0.50	0.00	0.00	0.00	0.00	0.50	0.00	0.00
COAL <sub>2</sub>	9.41	2.69	0.32	0.10	0.15	0.82	0.09	0.00	0.10	0.09	0.00
COAL <sub>3</sub>	3.64	1.35	0.26	0.59	0.11	1.91	1.23	0.64	0.09	0.00	0.29
CHAR <sub>C</sub>	1.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

Kmol j-th species per kmol of reference coal

### Nitrogen and Sulphur Distribution



Nitrogen Repartition*		Sulphur Repartition*	
$N_{CHAR} = 7.3 - 0.175 \times C_w + 1.12 \times 10^{-3} \times C_w^2$		$S_{CHAR} = 1 - S_{TAR} - S_{GAS}$	
$N_{GAS} = 1 - N_{TAR} - N_{CHAR}$		$S_{GAS} = -1.20 + 3.48 \times 10^{-2} \times C_w - 2.182 \times 10^{-4} \times C_w^2$	
$N_{TAR} = -6.56 + 0.177 \times C_w - 1.13 \times 10^{-3} \times C_w^2$		$S_{TAR} = -2.48 - 5.49 \times 10^{-2} \times C_w + 3.45 \times 10^{-4} \times C_w^2$	

\*Kg N or S in j phase respect nitrogen or sulphur content in coal parent.  
j = CHAR, TAR, GAS

#### Solid Phase CHAR: brute formula C<sub>1</sub>N<sub>x</sub>S<sub>y</sub>.

$$\alpha_{CHAR} = (100 - N_w - S_w) \times \sum_{i=1}^{N_{COAL}} \frac{\omega_{COAL,i}}{PM_{COAL,i}} \times \alpha_{COAL,i,CHAR,brute}$$

$$x = N_{CHAR} \times \omega_{COAL}^N \times \frac{PM_{COAL}}{PM_N} \times \frac{1}{\alpha_{CHAR}}$$

$$y = S_{CHAR} \times \omega_{COAL}^S \times \frac{PM_{COAL}}{PM_S} \times \frac{1}{\alpha_{CHAR}}$$

#### TAR Phase TAR: brute formula C<sub>x</sub>H<sub>y</sub>O<sub>z</sub>N<sub>s</sub>S<sub>t</sub>.

$$\alpha_{TAR} = \frac{(100 - N_w - S_w)}{PM_{TAR}} \times \sum_{j=1}^{N_{TAR}} \frac{\omega_{COAL,j}}{PM_{COAL,j}} \times \alpha_{COAL,j,TAR}$$

$$\phi_{TAR} = \sum_{i=1}^{N_{TAR}} x_{TAR,i} \phi_{TAR,i} \quad x_{TAR,i} = \frac{\omega_{COAL,i}}{PM_{COAL,i}} \times \alpha_{TAR,COAL,i}$$

$$k = N_{TAR} \times \omega_{COAL}^N \times \frac{PM_{COAL}}{PM_N} \times \frac{1}{\alpha_{TAR}} \quad j = S_{TAR} \times \omega_{COAL}^S \times \frac{PM_{COAL}}{PM_S} \times \frac{1}{\alpha_{TAR}}$$

#### Gas Phase: CO, CO<sub>2</sub>, H<sub>2</sub>O, C<sub>2</sub>H<sub>4</sub>, H<sub>2</sub>, HCN, H<sub>2</sub>S

$$\alpha_j = (100 - N_w - S_w) \times \sum_{i=1}^{N_{COAL}} \frac{\omega_{COAL,i}}{PM_{COAL,i}} \times \alpha_{COAL,i,j} \quad j = CO, CO_2, H_2O$$

$$\alpha_{H_2S} = S_{GAS} \times \omega_{COAL}^S \times \frac{PM_{COAL}}{PM_S} \quad \alpha_{HCN} = N_{GAS} \times \omega_{COAL}^N \times \frac{PM_{COAL}}{PM_N}$$

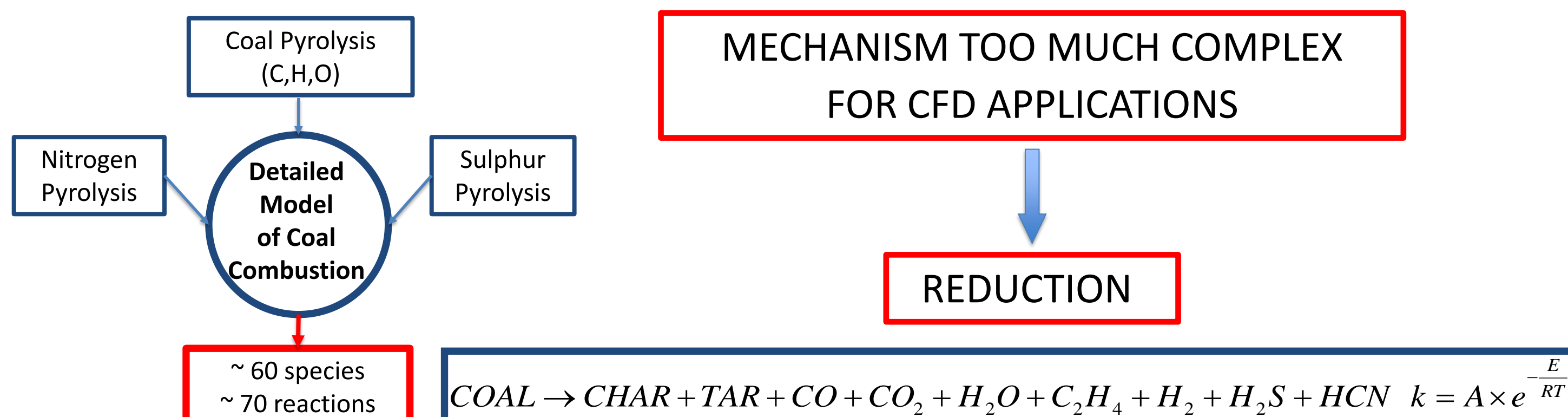
$$\Delta C = \omega_{C,coal} - PM_C \times \sum_{i=1}^{N_{COAL}} \frac{\omega_{COAL,i}}{PM_{COAL,i}} \times \alpha_{COAL,i,j} \quad \Delta H = \omega_{H,coal} - PM_H \times \sum_{i=1}^{N_{COAL}} \frac{\omega_{COAL,i}}{PM_{COAL,i}} \times \alpha_{COAL,i,j}$$

$$\alpha_{C_2H_4} = \frac{PM_{COAL}}{2} \times \frac{\Delta C}{PM_C} \times \frac{1}{2} \alpha_{HCN} \quad \alpha_{H_2} = \frac{PM_{COAL}}{2 PM_H} \Delta H - 2 \times \alpha_{C_2H_4} + \frac{1}{2} \alpha_{N,GAS} - \alpha_{H_2S}$$

#### Legend

- $\alpha_j$ : stoichiometric coefficient for j-th species in One Step Model
- $\omega_{COAL,i}$ : mass fraction of i-th reference coal [1]
- $\alpha_{COAL,i,j}$ : stoichiometric coefficient of j-th species for i-th reference coal [1]
- $PM_{COAL,i}$ : molecular weight j-th reference coal [1]
- $PM_j$ : molecular weight of j-th tar reference [1]
- $PM_{TAR}$ : molecular weight of TAR specie
- $x_{TAR,i}$ : molar fraction of i-th tar reference in tar mixture
- $\phi_{TAR,i}$ : atomic content in i-th tar reference and TAR
- $\alpha_{TAR,COAL,i}$ : stoichiometric coefficient of TAR<sub>i</sub> reference
- $N_w, S_w$ : mass % of N and S in coal
- $N_w, S_w$ : nitrogen and sulphur distribution in x phase, with x = CHAR, TAR, GAS
- $\omega_N, \omega_S$ : mass fraction of N and S in coal parent.

## GLOBAL MECHANISM and ONE STEP MODEL



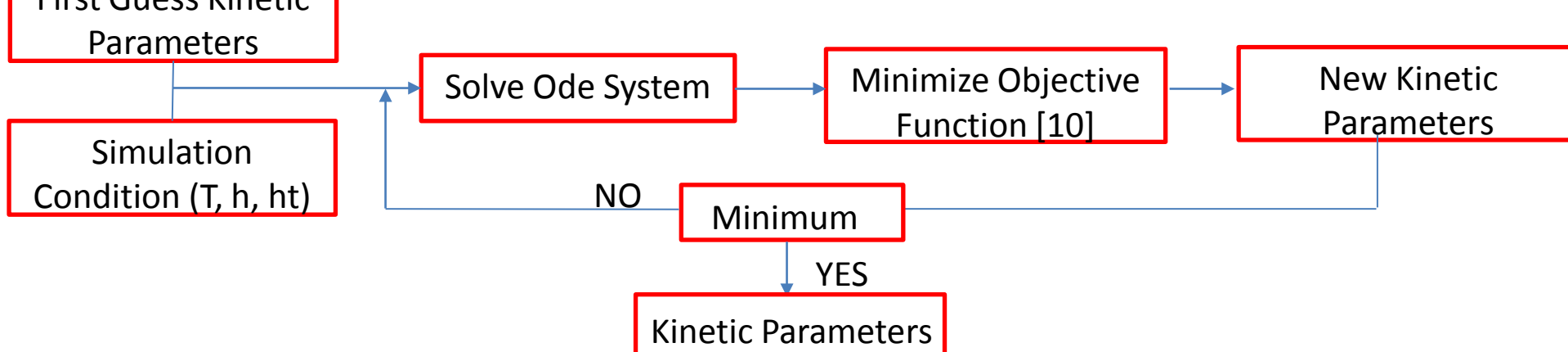
## KINETIC PARAMETERS OF ONE STEP MODEL

Detailed Mechanism  $\xrightarrow{\text{Oxy-Coal Conditions}}$  Dummy "Experimental Data"

Oxy-Coal Conditions:  $10^{4-5}$  K/s and  $T > 1400$  K  
Database: 13 Coals: from Lignite (65.4% C, daf) to Anthracite (93.7% C, daf)

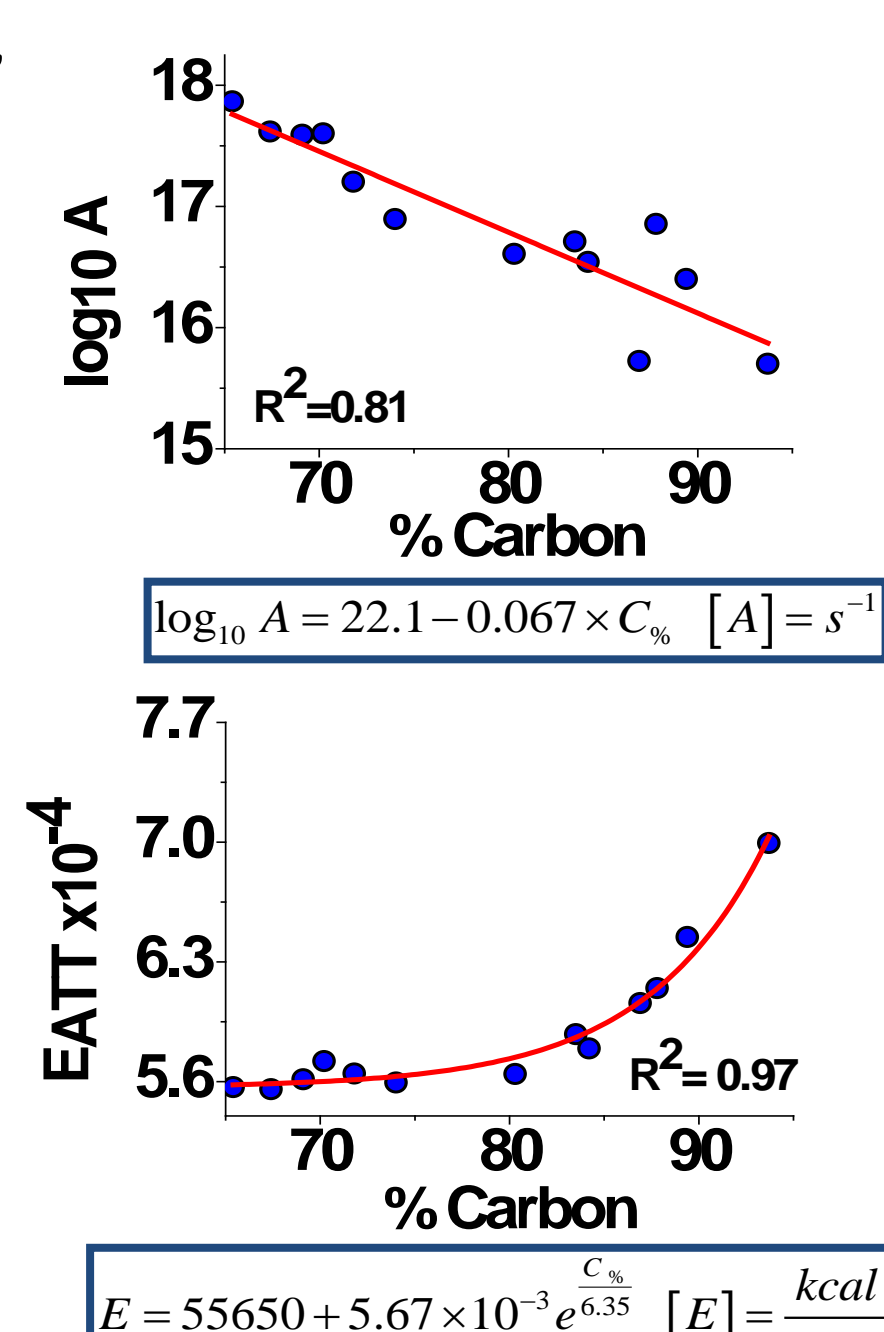
Non linear Regression Problem

$$S(\mathbf{b}) = \sum_{i=1}^{n_E} \sum_{k=1}^{n_y} [(y_{i,k} - g_k(\mathbf{x}_i, \mathbf{b}))^2]$$



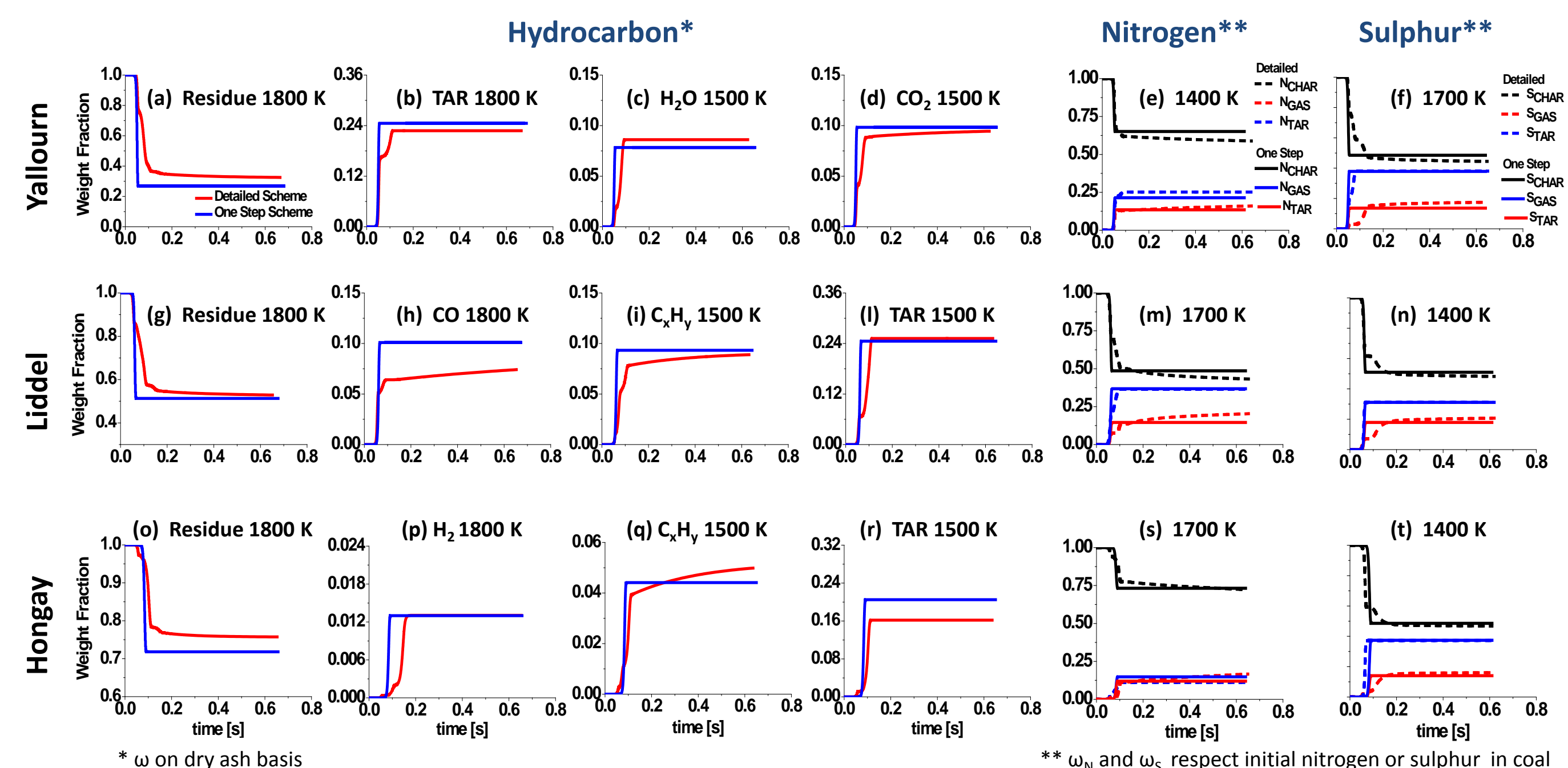
- $S(\mathbf{b})$ : objective function
- $n_E$ : number of experimental point
- $n_y$ : number of dependent variable  $y_i$

- $x_i$ : independent variable
- $\mathbf{b}$ : vector of parameters
- $g_k$ : kinetic equations



## COMPARISON BETWEEN MODELS

	One Step	% C, daf	CHAR	TAR	CO	CO <sub>2</sub>	H <sub>2</sub> O	C <sub>2</sub> H <sub>4</sub>	H <sub>2</sub>	HCN	H <sub>2</sub> S	A	E
Yallourn		65.3	2.219	0.143	0.721	0.222	0.432	0.323	0.632	0.0058	0.0013	5.7×10 <sup>17</sup>	55800
Liddel		83.5	4.146	0.144	0.356	0.022	0.074	0.317	1.209	0.0169	0.0034	3.6×10 <sup>16</sup>	58590
Hongay		93.7	5.880	0.128	0.066	0.000	0.007	0.150	0.634	0.0081	0.0026	7.4×10 <sup>15</sup>	70300



\*  $\omega_N$  on dry ash basis

\*\*  $\omega_N$  and  $\omega_S$  respect initial nitrogen or sulphur in coal

## CONCLUSION

In this work a simplified model for coal pyrolysis has been developed. The One Step model shows a satisfactory agreement with detailed models. Moreover the One Step model only needs the coal elemental composition as an input.

**Acknowledgments** This work is funded in the frame of the 'Accordo di Programma Ministero dello Sviluppo Economico- ENEA'

- [1] Sommariva S., Maffei T., Migliavacca G., Faravelli T., Ranzi E., Fuel, 89:318, 2010.
- [2] Maffei T., Sommariva S., Ranzi E., Faravelli T., Fuel(2011),doi:10.1016/j.fuel.2011.08.017
- [3] Chen J.C., Niksa S., Energy & Fuels, 6:254-264, 1992.
- [4] Perry S.T., Ph.D thesis, Brigham Young University, Utah, USA.
- [5] Basilakis R., Zhao Y., Solomon P.R., Serio M.A., Energy & Fuels, 7:710-720, 1993.

- [6] Hamby E.M., Ph.D thesis, Brigham Young University, Utah, USA.
- [7] Genetti D., Fletcher T.H., Energy & Fuels, 13:1082-1091, 1999.
- [8] Pohl J.H., Sarofim A.F., 16th Symposium on Combustion, 1977.
- [9] Fletcher T.H., Hardesty D.R., Sandia Report No. SAND92-8209, Pittsburgh, 1992
- [10] BzzMath 6.0 (Buzzi-Ferraris, http://homes.chem.polimi.it/gbuzzi/)